Tasks of nuclear physics ...

28450 Z/038/61/000/010/002/008 D291/D301

temperature of liquid helium can be started late in 1961. There are 14 figures and 15 Soviet-bloc references.

ASSOCIATION: Üstav jaderného výzkumu CSAV, Rez (Nuclear Research Institute Czechoslovak AS, Řež)

Card 6/6

BEM, Pavel; HABANEC, Josef; KARBAN, Oldrich; NEMEC, Jan

Measurement of proton polarization in elastic scattering on carbon. Jaderna energie 8 no.3:96-97 Mr '62.

17:00

Z/055/62/012/009/002/003

1046/1246

AUTHORS

Bém, P., Habanec, J. J., Karban, O. and Nemec, J.,

TITLE

Polarization of protons scattered elastically on carbon

PERIODICAL

Chekhoslovatskiy fizicheskiy zhurnal, v 12, no 9, 1962, 660-664

The polarization of protons scattered elastically on two carbon targets was measured for a cyclotron proton beam accelerated to 6.5 MeV. The angular distribution in the energy interval from 3.60 to 4.52 MeV was as follows $P(40^{\circ}_{lab}) = 0.30 \pm 0.05$; $P(45^{\circ}_{lab}) = 0.36 \pm 0.07$, $P(50^{\circ}_{lab}) = 0.33 \pm 0.06$, $P(60^{\circ}_{lab})$ = 0.20 ± 0.05. The results after scattering on one target are in good agreement with those given by Warner R E and Alford W P (Ref 6 Phys Rev , 114 (1959), 1338) There are 4 figures and 1 table

ASSOCIATION Institut yadernykh issledovaniy ChSAN (Institute of Nuclear Research Czechoslovak AS,

Rzhezh)

SUBMITTED

October 20, 1961

Card 1/1

BEM, P., HABANEC, J., KARBAN, O., NEMEC, J., PRESPERIN, V.

Polarization measurement of protons with 6.7 MeV energy scattered on carbon. Chekhosl fiz zhurnal 14 no. 64404-410 164.

l. Institute of Nuclear Research. Czechoslovak Academy of Sciences, Rez. $\,$

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l. Institute of la tear was the file dreamal value of the series Rez.
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L 18527-66 EWT(m)/EWA(h)

ACC NR. APS010229

SOURCE CODE: 02/0038/65/000/004/0144/0144

AUTHOR: Rem. Pavel; Habanec, Josef-Gabanets, Y.; Karban, Oldrich; Nemec. Jan 40. Nemets, Y.; Presperin, Vlastislav

ORG: Institute of Muclear Research, CSAV, Rez (Ustav jaderneho vyzkumu CSAV)

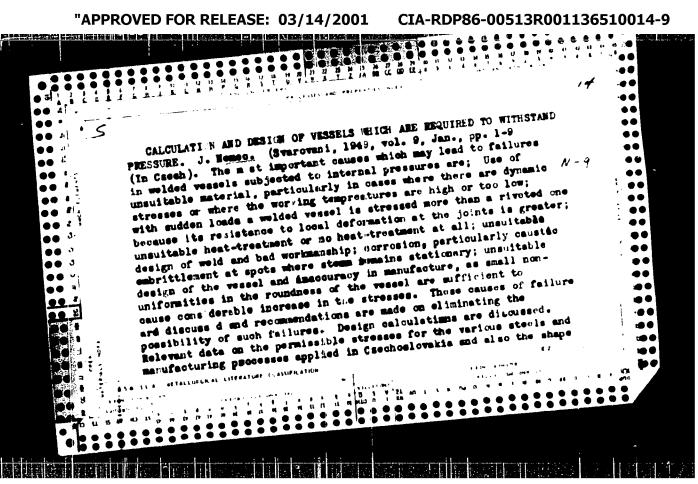
TITLE: Measurement of the angular distribution of the polarization of protons in the reaction C-12 (p. p) C-12 in the energy region of 6.0 - 6.8 Nev

SOURCE: Jaderna energie, no. 4, 1965, 144

TOPIC TAGS: proton polarization, elastic scattering, angular distribution, cyclotron, silicon, carbon, particle detector, particle accelerator target

ABSTRACT: INR Report No. 1064/64, published in Jaderna Energie only as Czech and Russian summaries (modified): The angular distribution of the proton polarization during elastic scattering was measured at six values of the energy in the region of 6.0-6.8 Mev. The energy source was the INR 120-cm cyclotron at Rez. The energy of the protons was reduced by means of aluminum and carbon films. The degree of polarization of the scattered protons was determined by the right-left asymmetry of the secondary scattering on the carbon target of the analyzar. The particles were region tered by silicon detectors with a surface barrier. The results of the Card 1/2

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NEMEC, J.

"Analysis of stresses in nonhomogeneous grains." Strojirenstvi, Praha, Vol. 4, No. 7, July 1954, p. 505.

SO: Eastern European Accessions List, Vol. 3, No. 11, Nov. 1954, I...

Nemec, J.

Powder cutting of high-alloy steels. p. 285. HJTNIK. (Ministerstvo hutniho prumyslu a rudnych dolu) Praha. Vol. 4, no. 9, Sept. 1954. Mechanical removal of waste from wire of low-carbon steel. p. 286.

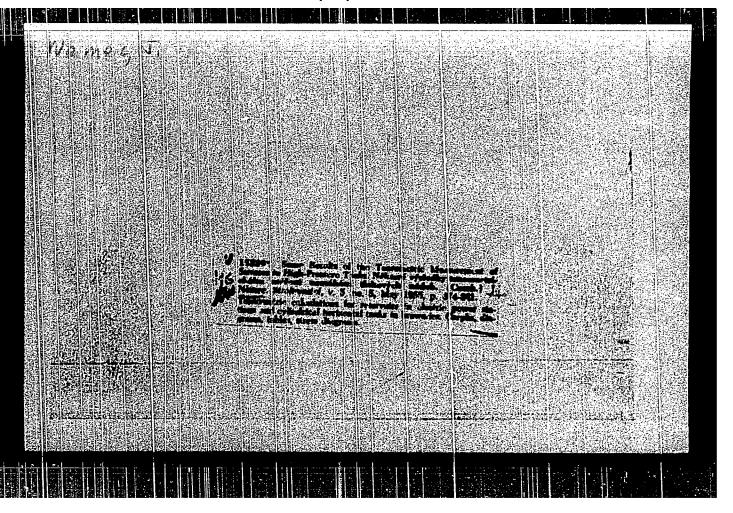
Source: EEAL LC Vol. 5, No. 10 Oct. 1956

NEMEC, J.

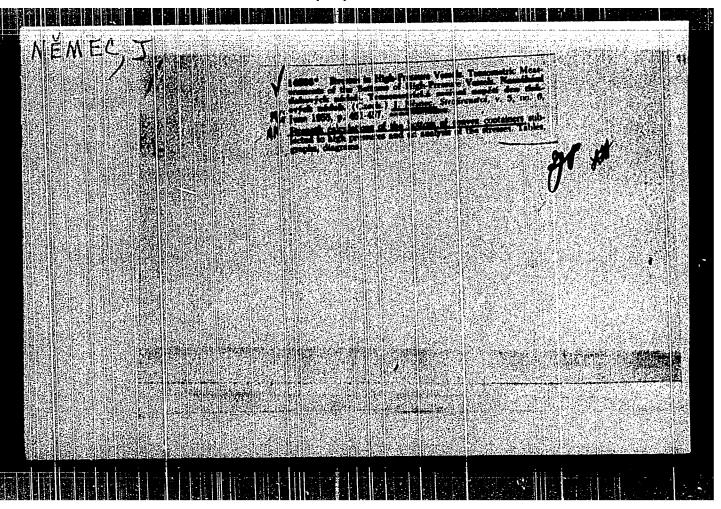
Zednik, V. Testing impact ductility, p. 766. STROJIRENSTVI, Prague, Vol. 4, no. 10, Oct. 1954.

SO: Monthly List of East European Accessions, (EEAL), LC, Vol. 5, No. 6, June 1956, Uncl.

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Strain on vessels with rotary asymmetric necks, p. 538, STROJIREVSTWI (Ministerstvo strojirenstvi) Praha, Vol. 5, N. 7, J ly 1955

SOURCE: East European Accessions List (FEAL) Library of Congress, Vol. 4, No. 12, December 1955

NEMEC. J.

Calculating the cutting effect of a v-shaped joint of a pressed-in hub. g. 3.
(Strojirenstvi, Vol. 6, No. 1, Jan 1056, Fraha, Czechoslovakia)

SO: Monthly List of East European Accessions (EMAI) IC, Vol. 6, Fo. 6, Aug 1957. Uncl.

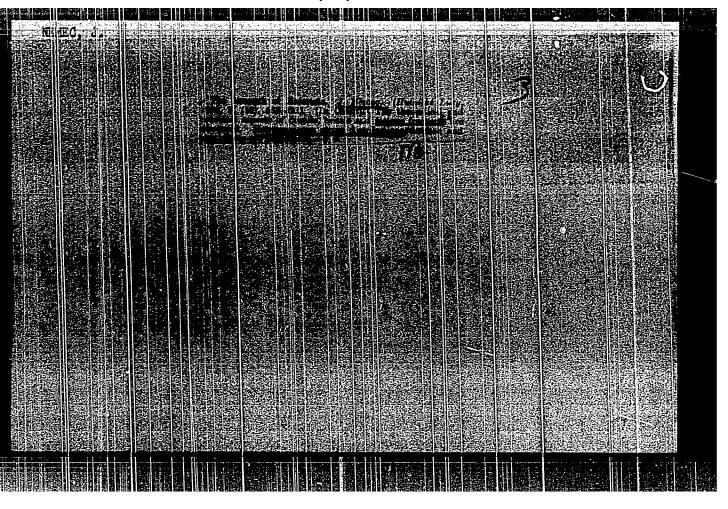
Nemec, J.

Nemec, J. Influence of the size of a spare part on its solidity. p. 257.

Vol. 7, no. 5, 1956
STROINOELEKTROTECHNICKY CASOPIS
TERROLOGY
Czechoslovakia

So: East European Accessions, Vol. 6, May 1957

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	2338 (Czech: Structh Limits of Mai rist Meza stay Perusul miterisis: Jafoliae Nemec. Hunk id Listy, v. 11; no. 10. Oct. 1916, p. 535-191. 3 Shows the development of plastic and brittle fractures by means of this emigy balance, and conditions which we responsible for their origin.

Measuring the pressure of presses. p. 227. (Strojirenstvi, Vol. 7, No. 3, Mar 1957, Praha, Gzechoslovakia)

So: Monthly List of East Euroneum Accessions (EEAL) LC, Vol. 6, No. 8, Aug 1957, Encl.

HEMES, J.

Improvement of calculation methods is a prerequisite for reducing the weight and increasing the dependability of machinery and constructions. p. 321. (Strojirenstvi, Vol. 7, No. 5, May 1957, Praha, Czechosi: rakia)

SO: Monthly List of East European Accessions (EEaL) LC. Vol. 6, No. 8, Aug 1957. Uncl.

NEMEC, J.

Effect of the shape of steel parts on heat stress relaxation. p. 403.

(Strojirenstvi. Vol. 7, no. 6, June 1957. Prama, Czechoslovakia)

S0: Monthly List of East European Accessions (EEAL) LC, Vol. 6, no. 10, October 1957. Uncl.

Use of new theoretical and experimental methods is designing anothery.

...61. (SINOUINGENTAL) (Praha, Ozeonoslovakia) Vol. 5, 12, Lec. 1.17

Dynamic strength of rolling stock under a mained virying strut; c.

3. 863. (SIGMICTOTVI) (irain, Dzechoslovakia) Vol. 7, no. 12, Lec. 197

30: Konthly Endex of East European Accession (CEAI) 10 Vol. 7, No. 5, 199

NEMEC, J.

CZECHOSLOVAKIA/Bolid State Physics - Mechanical Properties of Crystals and Poly-Crystalline Compounds

E-9

Abs Jour

: Ref Zhur - Fizika, No 1, 1958, 1102

Author

: Hemec, Jaroakav

Inst

: Higher School for Iron Working, Pragues, Czechoslovakia

Title

: Plastic Stressed State in Steels.

Orig Pub

: Extniche listy, 1957, 12, 50 4, 315-324

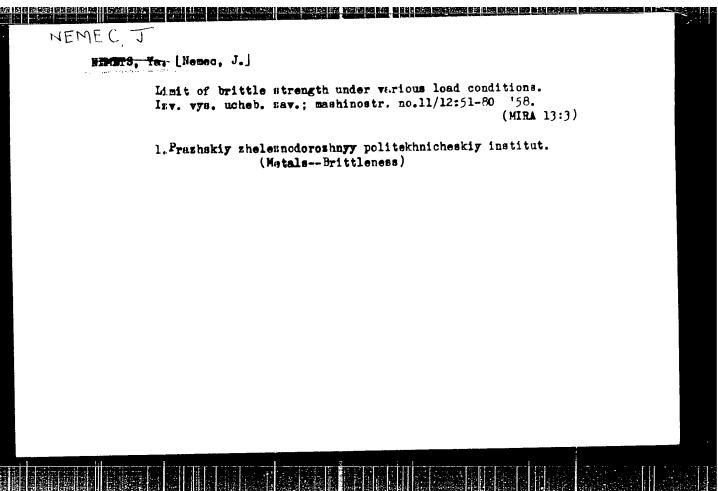
Abstract

: The author considers the processes that precede the destruction of the adhesion forces in deformed steels, and raises the problem of the possibility of calculating the plastic stressed state in inhomogeneous materials. An investigation is made of the dependence of the static strength of steel on the fundamental physical properties that characterize the deformation of the ferrite. The mathematical foundations and deductions of the theory of

Card 1/2

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NELEC, J. Theory of the stringth Hills of strels. 1. 1111.

monthly list of East European Accessions (LIAI) LC Vol. 6, no. 5 Lay 1959, nolass.

NEMETS, Yaroslav [Nemec, Jaroslav], prof., doktor tekhn.nauk (Chekho-slovakiya)

Selecting admissible stresses in high-pressure pipes used in hydroelectric power stations. Vest.mash. 38 no.12:3-7 D '58.

(MIRA 11:12)

(Pipes) (Strains and stresses)

NEMEC, J.

"Effect of shape, machining, and heat on the values of allowed strains in parts." p. 409.

STROJIRENSTVI. (MINISTERSTVO TEZKEHO STROJIRENSTVI, MINISTERSTVO PRESNEHO STROJIRENSTVI A MINISTERSTVO AUTOMOBILOVEHO PRUMYSLU A ZEMEDELSKYCH STROJU.) Praha, Czechoslovakia, Vol. 9, no. 6, June 1959.

Monthly List of East European Accessions (FEAI), LC, Vol. 8, No. 9, September 1959. Uncl.

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Z/038/60/000/008/001 001 A201/A026

26.2200

AUTHOR:

Němec, Jaroslav

TITLE:

Strength of Nuclear Reactor Vessels 19

PERIODICAL: Jaderna energie, 1960, No 8, pp. 254 - 266

TEXT: The article presents an analysis of strength limits of large reactor pressure vessels. The analysis was undertaken in preparation of the designing of the pressure vessel for the first Czechoslovak nuclear power station. In particular, the article investigates the correlation between vessel size and radiation concentrations; the brittle strength of the vessel; the influence of thermal stresses on the vessel strength; and the influence of cyclic stresses on the service life of the vessel. Relations are deducted for the calculation of the shape strength of the vessel and for the determination of limit stresses leading to the development of sudden critical ruptures. The pressure vessel of the Czechoslovak nuclear power station will be produced of Type 13030 fine-grained steel. For this steel type, the critical integrated neutron flux at which the vessel material brittleness will reach a non-permissible value is estimated to be about 5 · 10¹⁸. This value just about approaches the upper limit of the in-

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Strength of Nuclear Reactor Vessels

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tegrated neutron flux of 10^{18} - 10^{21} to which the vessel will be exposed during a 30-year operation at an expected instantaneous neutron flux of 109 - 1012 neutrons/cm2/sec. Therefore, a better thermal shield will have to be designed, especially since the temperature range, at which the damaging effects of the neutron flux for this steel type are most pronounced, is between 100 and 200°C, which is exactly the temperature range at which the vessel of the Czechoslovak nuclear power station is designed to operate. From the above analyses, the following directions for reactor pressure vessel design and fabrication are deducted: 1) In designing and calculating the strength of reactor vessels it has to be considered that during long-term operation the plastic properties of the material will deteriorate and the limit-stress value at which cohesion defects start developing will gradually decrease. The extent of these unfavorable property changes will increase with the increasing wall thickness, integral neutron flux and stress concentrations; with more frequent and extensive changes of pressure and temperature; and with more numerous incipient material defects. 2) Static properties of material, as established by conventional test methods on small specimens, do not provide a satisfactory basis for the calculation of safety factors in reactor vessel design. 3) The stress-concentration and notch effects will increase with the increasing thickness of the vessel wall. 4) The effect of cyclic stresses will be the greater the more brittle is the material

Card 2/3

Strength of Nuclear Reactor Vessels

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and the more complicated the vessel shape. 5) In stress calculation, due consideration is to be given to the internal and thermal stresses to which the vessel will be exposed. 6) The calculation of the permissible stress and stress-concentrations is a complex problem which cannot be solved by a mere extrapolation of experience gained with thin-walled pressure vessels of smaller sizes 7) Prior to the full-scale operation a series of verifying measurements and tests will have to be carried out in order to determine the actual safety of the vessel. There are 20 figures, 1 photo and 24 references: 9 Czechoslovak, 2 Soviet, 11 English and 2 Unidentified.

ASSOCIATION: Vysoká škola železnićní (Railroad College)

Card 3/3

PHASE I BOOK EXPLOITATION

CZECH/5191

Němec, Jaroslav, Professor, Engineer, Doctor of Sciences

Tuhost a pevnost ocelových částí (Rigidity and Strength of Steel Parts) Prague, Nakl. Československé akademie věd, 1961. 567 p. 1,500 copies printed.

Sponsoring Agency: Československá akademie věd. Sekce technická.

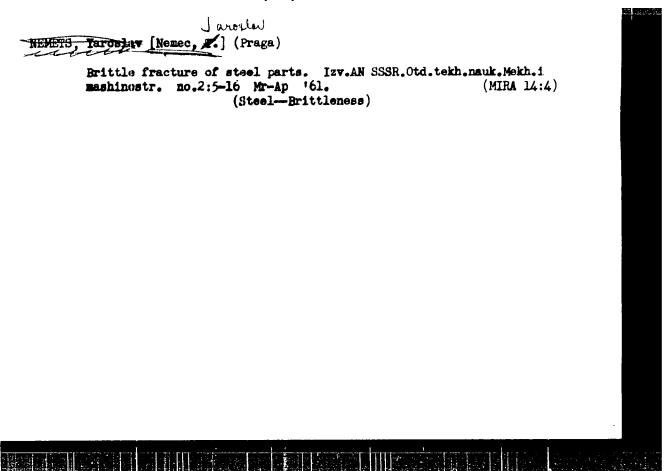
Scientific Ed.: Jaroslav Kožešník, Academician; Scientific Reviewers: Ladislav Jeníček, Professor, Doctor, Engineer, and Cndřej Puchner, Professor, Engineer, Doctor of Sciences; Ed. of volume: Antonín Burda; Tech. Ed.: František Končický.

PURPOSE: This book is intended for technical personnel concerned with research, development, and production in the machine industry.

COVERAGE: The following questions concerning steel parts and constructions are discussed: fractures, deformation processes, theory of plasticity, endurance at elevated temperatures, brittle

Card 1/9

Rigidity and Strength of Steel Parts CZECH/51	.91					
fracture, and fatigue strength. The author thanks J. Kožešník, L. Jeníček, and O. Puchner for their advice and editorial assistance. There are 266 references: 71 Czech or Slovak, 46 Soviet, 102 English, 36 German, 3 French, 2 Polish, 1 Rumanian, and 5 others.						
TABLE OF CONTENTS:						
Foreword	5					
List of the Most Important Symbols	10					
1. Introduction 1.1 Objectives and development of the science of rigidity, strength, and durability of steel parts and constructions	17					
1.2 Concise review of the development of the engineering science of the strength of materials 2. The Appearance of Fractures in Steel Parts	17 22 29					
Card 2/9	-7					



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18000

AUTHOR: hěmec, Jaroslav

TITLE:

Development of material cracks in an inhomogeneous

field of internal stresses

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FEATODICAL:

Jaderná energie, no. 4, 1962, 117 - 121

TEXT: The article investigates the laws governing the levelopment of cracks in todies with a nonuniform distribution of residual stresses featuring high local-stress concentrations. The purpose of the study is to provide a tool for analyses of crack-formation, que to fabrication processes, so as they may be eliminated by selecting proper technological processes (heat treatment, welding methods) which are compatible with the strength of the bodies. Two basic causes of plane stress caused in a thin slab by rotationally-symmetrical deformation effects (spot welds or local flame heating), and by a longituainal stress field of parabolic shape (internal stresses in longitudinal welds or thin walls or longitudinal material defects) respectively,

Card 1/2

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Development of material cracks ...

are investigated. It is found that the ratio of the critical length of the crack or defect to the dimensions of the region of tensile stress plays an important part. Also, the condition of crack lability is defined. The study is of importance for determining the dangerousness of cracks in relation to the dimensions of the area affected by internal tensile stresses, and may find application especially in the new fabrication techniques of extra-large bodies. There are a figures (Technical Editor: V. Horak).

13

ASSOCIATION:

Fakulta technické a jáderné fyziky JVUT, Praha (Bepartment of Technical and Auclear physics, Czech Institute of Technology, Prague)

Card 2/2

24285 Z/032/61/011/008/004/009 E073/E535

188200 also 2807

AUTHOR: Nemec. J., Professor Engineer Doctor of Science

TITLE: Evaluation of creep test data

PERIODICAL: Strojírenství, 1961, Vol.11, No.8, pp.613-616

In evaluating the scatter of results relating to creep tests, attention is paid not only to determining the average probable values but also to the possibility of determining the minimum values. It is thereby not possible to use the symmetrical law of distribution of the values according to the Gauss curve, since the application of this law would mean that the occurrence of the limit state can never be excluded with absolute reliability. Use of this law would also be contrary to the conceptions of the dislocation theory of creep. For homogeneous creep the real distribution curve is more likely to be the one in dashed lines of Fig.1, since the limit state cannot be achieved under certain minimum stress and minimum testing time. Since in real components creep under normal conditions is usually the simultaneous result of two methods of creep, a more complicated characteristic can be anticipated, namely, that shown by the dash-dot curve in Fig.1. Card 1/4

Evaluation of creep test data

24285 2/032/61/011/008/004/009 E073/E535

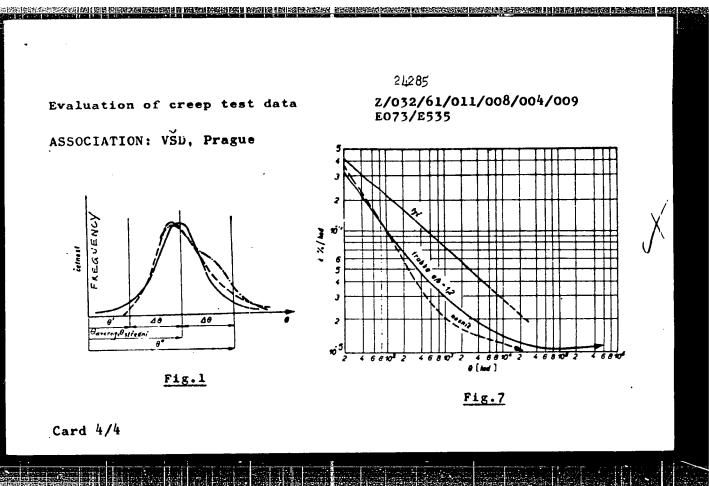
Therefore, analyses based on the Gauss law of distribution give results which are doubtful. Of still greater importance is the fact that excessively simplified relations between time $\, \, \Theta \,$, stress o and temperature T are applied, without taking into consideration geometrical factors and stress distribution. The results are frequently applied to the calculation of components using particularly the Larson-Miller equation, which is an empirical one and does not take into consideration the real conditions pertaining to creep in polycrystalline metals and alloys. It is pointed out that the speed of creep is not constant and it decreases with loading time. This conclusion is true even for smooth specimens, for which, according to R. Pokorny, the reviewer of this article, the dependence of the creep speed on time is complicated (the actually measured results for one Czech steel are given). The standard method is particularly inapplicable for parts of complicated shape, since the dependence of the creep speed on the loading time is clearly a function of the geometrical shape and its stress state. The physical process of creep should be subdivided into two phases; in the first the creep speed decreases Card 2/4

24285 '

Evaluation of creep test data

Z/032/61/011/008/004/009 E073/E535

as a result of equalization of stress peaks, in the second large plastic deformationsoccur (not taking into consideration tertiary creep), which result in changes in the shape of the body, thus generating internal stresses, which in turn lead to an increase in the creep speed. The author concludes that correct calculation of the strength and rigidity of machine parts operating under conditions of creep has to be done on the basis of the following principles: a) the creep and creep strength tests should not be carried out on smooth specimens but on sections subjected to bending stresses and on tubes which are subjected to internal pressures or on bodies which are subjected to combined stresses. Calculated values are given for a concrete case in which the creep results of a smooth specimen (tyc) are compared with those obtained for a tube (trubka) and a section (nosnik), Fig.7 (ϵ ,%/hour vs. O, hours). b) Extrapolation should not be made on the basis of Larson-Miller or Kauzmann formulae; geometrical factors and changes in creep speed should be taken into consideration. c) More exhaustive studies should be made of stress relaxation processes. There are 9 figures and 2 references: 1 Czech and 1 English: Rimrott, F.P.J., Journal of Applied Mechanics, ASME, series E6.1959. Card 3/4



19.8200

36739 Z/032/62/012/001/001/007 E073/E635

AUTHOR:

Nemec, J., Professor, Engineer, Doctor of Science,

(Prague)

TITLE:

Limit-strength states of large machine parts and

vessels stressed at low temperatures

PERIODICAL: Strojirenství, v.12, no. 1, 1962, 11-15

TEXT: Sudden brittle fracture may arise even at stresses which are fully permissible according to valid specifications. These appear to arise primarily in large parts, usually in welded structures and vessels. The danger of damage increases with increasing dimensions and complexity of shape of the body, decreasing temperatures of the material and increasing internal stresses caused by welding. In the present paper the author has studied the factor of size and the influence of internal stresses in weld joints for the purpose of determining the basic decisive parameters of the limit state of the brittle strength with regard to the shape of the body, dislocation andthe length of its welded joints. It is assumed that the part is in operation in a state in which only rapid brittle fractures can occur, i.e. that

Z/032/62/012/001/001/007 E073/E635

Limit strength states of large ...

the temperature of the material is below the transition temperature, a condition which is frequently fulfilled in normal operation.

Two main factors influencing brittle fractures from the point of view of size and shape of the body are considered; elastic energy stored in the body, particularly with reference to welded vessels and the relation of shear stress to maximum normal stress.

Conclusions reached from the analysis indicate that at low temperatures, when the possibility of sudden brittle fracture must be considered, tests carried out on small specimens of the material have no real value. Influence of geometrical factors, such as size and shape as well as internal stresses, is considerable. These factors, derived in the paper, are relative only, giving a comparison of the limiting values of brittle strength. Actual values are influenced by the constants of the material and

Card 2/4

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Limit strength states of large ...

To such tests scaling must be determined or verified from tests. is applicable and it is here therefore that the geometrical parameters play their major part. Standard criteria, applicable to smaller bodies and working at normal or raised temperatures, cannot be applied to the design of large vessels operating at low temperatures, i.e. in the zone of brittle fractures. Such vessels are frequently encountered in the chemical or power generating Conventional mechanical properties of the material can no longer be used when computing the safe stresses of such Internal stresses and the level of elastic energy stored in the material have a considerable influence and must be taken into account. The properties of the material are best characterised by the quantity K, kg/cm2, i.e. the specific energy per 1 cm2 of the fractured surface, which in metals is determined by the specific deformation energy per 1 ${\rm cm}^3$ required to reach the limit-strength state of the material. The quantity K is a

Card 3/4

Z/032/62/012/001/001/007 E/073/E635

Limit-strength states of large ...

material constant which depends on the temperature and the velocity of propogation of a crack and, to a certain extent, on the shape of the cross-section. Comparison of test results carried out in the Soviet Union and Czechoslovakia on large specimens on which sudden brittle fracture was produced with appropriate notch-impact values, gave an average value of $K=20~a_{\rm k}$ obtained for steel bodies at normal temperature. There are

Card4/4

NEMEC, J., prof., ins., Sc.Dr.

The Scientific Conference of the Engineering Faculty of Higher School of Technology in Brno. Strojirenstvi 12 no.1:69 Ja 162.

Use of mathematical machines in machinery industries. Strojirenstvi

Use of mathematical machines in machinery industries. Strojirenstv... 12 no.4:241-242 Ap 162.

77165 1 z/032/02/012/005/002/004 5073/5335

107400

AUTHOR: Nemec. J. Professor Engineer, Doctor of Sciences

TITLE: Study of the propagation of fatigue cracks in bodies

PERIODICAL: Strojirenství, v.12, no. 5, 1962, 346 - 369

The influence of various factors on the spreading in TEXT: width and depth of cracks is expressed by means of intheratically derived relations, paying particular attention to cases in unich the material is subjected to alternate stresses. Differences in the behaviour of hard and soft materials are pointed out. The progress of the cracks is illustrated on the example of a cylindrical rod subjected to bending during rotation and a prismatic rod subjected to repeated bending. The crac's for a at the surface and, during the first stage, spread prodominantly inside the surface layer. When the entire surface layer is damaged they spread inwards and the depth of the crack increwes progressively to a critical value. The plot, Fig. 4, shows the main stages of development of a crack. Up to a certain nucler of stress cycles the damage to the material accumulates in the exposed spots and manifests itself only after N load Card 1/5

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D075/335

Study of the propagation

cycles in the form of a visible crack or cracks. Then, this crack propagates inside the surface layer and other cracks may also form there. Up to a certain, relatively large, number of cycles the depth of the damaged layer f = S remains unchanged. When the cracks—eventually interconnect and the main part of the surface layer, which is exposed to unfavourable tensile stresses, is damaged a change occurs; on reaching N^* load changes the third phase of breaking-up of coherence sets in. It was established by numerous measurements and tests that from this time onwards the relative depth of the crack f showed a linear increase with the number of further load cycles. The crack increases up to $N_{\rm ER}$ cycles when a critical depth of the crack f is achieved, at which

time there will be a sudden brittle fracture through the remaining cross-section $\ell=h$. The more sudden the clouder in load, the smaller will be the number of load cycles N and $N_{\rm sign}$ and the more rapid will be the spreading inwards. The

Card 2/5

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Study of the propagation

critical depth $\ell_{\rm KR}/h$ of a crack will decrease with increasing stress. On the basis of numerous results from fatigue fractures and fractures of test specimens, it was found that for soft constructional steel at normal temperatures the average work of plastic deformation required to produce a fracture per $1~{\rm cm}^2$ of the area of the final fracture was $K=100-150~{\rm kgcm/cm}^2$ for static loading and $K=30-60~{\rm kgcm/cm}^2$ for impact loading. An empirical formula for determining the size of the crack, which starts spreading on further cyclic loading,

X

is:

 $\sigma^3 z = c$.

where σ is the nominal stress assumed in the calculations, ℓ is the characteristic length (for instance, depth) of the crack.

Of the crack.

C is a constant depending on the structure of the material, particularly on its surface layer. The quantity expressing Card 3/5

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Study of the propagation

this constant is analyzed and it is concluded that the criterion $\sigma\ell=C$ is not reliable enough for determining the stability of cracks. The author derives the following empirical relation for carbon steels:

$$\frac{N^*}{N_{KR}} \ge 0.2 \frac{5}{\sigma_c}$$

He concludes that the dependence of the depth of the crack or of the relative area of the crack on the number of load cycles is a complicated one, indicating the different stages of development of the crack. Therefore, the service life of components cannot be calculated from a single analytical relation and is not determined by a single material constant. Further verification and development of the calculation method will permit determining the permissible state of cracks for a predetermined increase in the number of load cycles,

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Study of the propagation

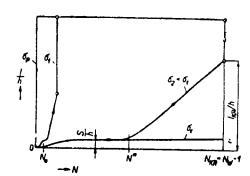
i.e. for a certain service life. It will also be of interest to study the control of the process of development of surface cracks by suitable surface treatment.

There are 6 figures.

ASSOCIATION:

Fakulta technické a jaderné fyziky, ČVUT, Praha (Department for Technical and Nuclear Physics, ČVUT, Prague)

Fig. 4:



Card 5/5

NEMEC, J., prof., ins., dr., Dr.Sc.

Development of technical education. Strojirenstvi 12 no.10:721-722 10 0 '62.

1. Ceske vysoke uceni technicke, Praha.

KUPKA, Ivan, NEMEC. Jarceley; STEPANEK, Stanislav

Internal stresses in making pressure vessels for nuclear

reactors. Jaderna energie 9 no.5:146-155 My '63.

1. Zavody V.I. Lenina, Plzen.

Z/032/63/013/001/004/004 E073/E183

AUTHOR: Mesec, J.; Professor of Engineering, Doctor of Sciences
TITLE: The resistance of large parts to brittle fracture
PERIODICAL: Strejirenstvi, v.15, no.1. 1965, 52-55

TEXT: In an earlier paper the author showed that there is a definite relationship between the geometry of a part and its mechanical properties, and that this relationship is important from the point of view of determining the limit state. Fracture will be facilitated by low values of the elasticity modulus B and energy required for producing a unit area of the fracture K, and by high yield point of and large characteristic dimension of the bady L. To initiate a brittle crack in steel bodies the following conditions have to be fulfilled; a) there must be a critical motch effect aur of the initial defect or notch; b) the localised yield point must increase to reach, before plastic deformation can occur, a sufficiently high local normal stress of; c) the total work of all sliding actions in the exposed spot (generally the work of local plastic deformation) must be greater than the energy required te form now free surfaces of the size A? in the body: Card 1/5

The resistance of large parts to ... 2/032/63/013/001/004/004 8073/2183

 $\Sigma L_{i} \geq L_{i}$

List composed of the local deformation work required to reach the limit state \$\hat{\mathcal{h}}_0\$ (s - limear dimension affected by the local plastic deformation) and the energy which is required for accelerating the propagation of the crack and the development of the crack with the limit velocity \$v_0\$ for the given size of the part \$L\$ and its stress state. The average value of \$L\$ for the formation of a fracture of area \$l\$ cm^2\$ is determined approximately from tests with large parts at a constant temperature. To facilitate brittle fracture the tests are carried out at low temperatures. The origin of the fracture will be a sharp notch and the initial stress increase as well as the acceleration of the crack propagation is facilitated by impact on a wedge inserted into the notch. Then the dimensions and the geometry of the formed crack are studied. To facilitate evaluation of the results of such tests the conditions are investigated for a specimen without internal atresses; as illustrated in Fig.1. It is assumed at first that the length of the specimen is less than its width and that a Card 2/5

The resistance of large parts to ... Z/032/63/013/001/004/004

crack has developed. The expressions derived will be generally valid if the influence of elastic deformation and of some other factors is taken into account, The critical stress for the crack to propagate is:

 $\begin{array}{c|c} & & \text{and } & \text{i.e. } (\mathbf{n}, \ell)^2 \\ & & & & \\ & & & & \\ \end{array}$

where g 2s and x = P/h is the specific transverse force at the sides of the notch or of the crack produced by impact on the wedge. The higher the value of x for a given gr. the lower will be the necessary length (gr of the crack required for it to propagate; Parts ande of material with a high yield point and a low value of K are particularly sensitive to brittle fracture. The product K x E is virtually constant for any given material, whilst gli is the level of the limit electic stress of a given part of dimension L. The parameter KR/gL is the ratio of the "material constant" to the specific energy of electic stress of a body of a certain size. The higher the intensity of the impact,

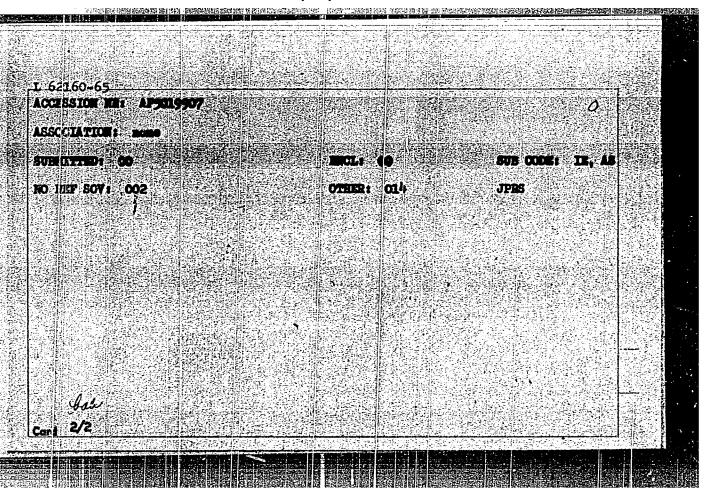
Z/032/63/013/001/004/004 E073/E183 the lower will be the motch effect required to achieve crack propagation. The influence of transverse shear stresses on the elastic deformation is disregarded in the first part of the analysis, but this is not permissible for long specimens for which a correction factor can be derived. The influence of transverse forces litereases the size factor and reduces the limit stress. The study is based on a crack emanating from the surface but it can be modified to apply to a centrally located initial crack or north mucleus. The main purpose of the studies was not to determine quantitative formulas, but to derive basic expressions for estimating the parameters of and evaluating experimental data on brittle fracture of large specimens, and for determining the 50 similarity laws and the basic relations governing material There are 2 figures ASSOCIATION: CVUT, Praba (CVUT; Prague) Card 4/5

L 11020-65 EWT(m)/EPF(in)-2/I/EWP(k)/EPA(bb)-2/EWP(v)/SWP(t)/EWP(b) PI-4/Pu-4 SSD/AEDC(b)/AFWL/BSD JD/HM ACCESSION NR: AP4044866 2/0038/64/000/009/0322/0336 AUTHOR: Haper, Josef (Khauyer, Y.); Havel, Stanislav (Garel, St.); Nemac. Jaroslay (Nemets, Ya.); Stepanek, Stanislay (Shtepanek, St.) TITLE: Pressure vessel of the first (sechoslovak nuclear electric power plant Jagerna energie, no. 9, 1964, 322-336 SOURCE TOPIC TANS pressure (these la longerton steel possible steel, a welding, impact strength, electroslap welding, automatic welding, nuclear ABSTRACT: A survey is made of investigations and determinations of the optimum dispussions and shape of the most stressed parts of the pressure vessel of the firm Czechoslovak nuclear power plant, in particular, the cover, the bottom, and the inlet and exit flanges of the cooling gam tube. The reactor is D₂C moderated and CO₂ cooled. For a power cutput of 150 Mi its diameter is about 5 m and altitude 20 m, and for an operating pressure of 65 at the cylindrical walls must be 150 mm thick. The pressure vessel is made of low-Card 1/2 the second of the second second

ally impact strength, and hows that both manual ar	ll-grain, non-aging steel having good mechanical properties, espec- t strength, and a minimum of permissible defects. The investigation both manual are welding and automatic electroslag welding can be						
uccessfully used for well	or investigating brittle had of the pressure vessel	wires and the results are	(1)				
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ACCIZATION NR: AP5019907		C2/OC32/64/O14/	012/0910/0915	
AUTHOR: Nemec, J. (Professor, Engin	eer, Doctor of	sciences) (Pre	Ena)	
TITLE Development of cracks in ste	el parts		17	
SOURCE: Strojirenstvi, v. 14, no. 1		n (t	B	
NOPIC TAGS: steel, mechanical engin Tracture	eering, metal	fatigue, metal	stress; metal	
Abstract (Author's English sum analyzes the nature and mechan arts under repeated and fatigated by the results of certain plearly a new approach to the calculations. The new theorie on the effect of microscopic caterial and introduce new electical strength. The conclusives of calculation ully justified.	recent reservoice stress. recent reservoice of separt from cacks presented into the constitutions indicated series.	ing in steel the study is arch work in ifety and star convention; in the strice calculations that some	machine domin- dicating rength al views ucture of on of of the	
ully justified. Orig. art. has	l figure, u	ormins, 5 gra	plis, and	

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NEMEC, Jaroslav, prof., inz., doktor ved.

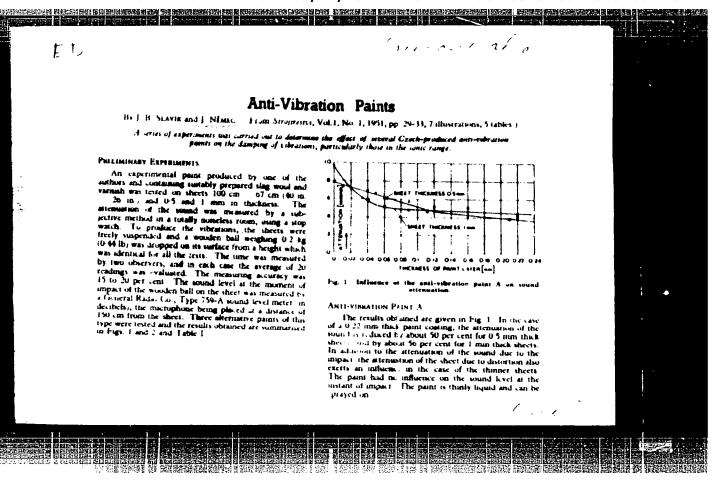
Saving of construction materials and the quality of products. Podn org 18 no.2: 49-52 F-64

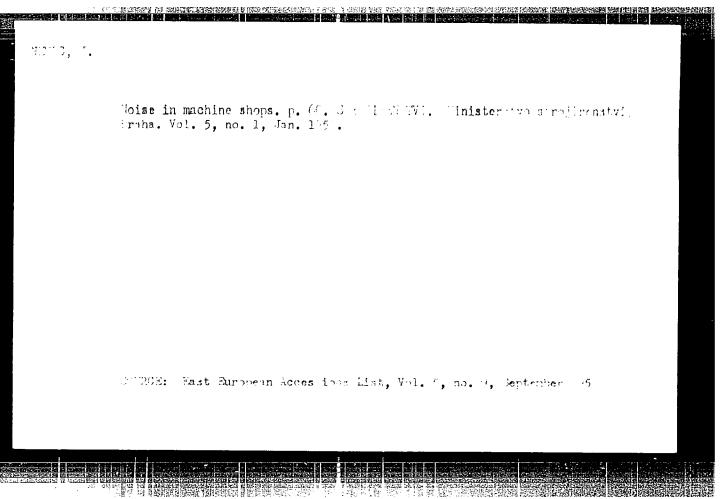
1. Faculty of Technical and Nuclear Physics, Czech Higher School of Technology, Prague.

NEMEC, Jaroslav

Maintenance and planned checking and repair. Elektrotechnik
20 no.1:24-25 Ja '65.

1. Repair Shop of the Svit National Enterprise, Gottvaldov.





OZTIHOSLOVANIA/Abousties - - sour il Problems 7.1 Abs John: All Lare + 2-Zat, 500, 100, 0011. Author :c Jurosi .v 13:1 īltlu : Units and inthoducer literania, Louisia, 2 Sound Orig Pub : Al boproud; obtor, 1963, to, 35 7, 2-13-2-10 Abstract : In composition with the find for many lization or sources a sour sounds, our lation of relative grinding I unies for the communit (phon, to a) and the redefinations. A some received rilbit dicicila, pacia, and so as, and remained describing of an area are discretiff, when were inflation on the toloristic last, d. - C.G. Kir A ...

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NEMEC. J.; RANSDORF, J.

Present problems of protection against the noise. p. 107

ZDRAVOTNI TECHNIKA A VZDOCHOTECHNIKA. Praha, Czechoslovakia. Vol. 2, No. 3, 1959

Monthly List of East European Accessions (EEAI), LC. Vol. 8, No. 9, September 1959 Uncl.

NEMEC, J.

Sound silencers and their application in silencing engine noise, p. 43

Ceskoslovenska vedecka technika spolecnost pro zdavotni techniku a vzduchotechniku, Praha, Czechoslovakia, Vol. 4, 1959.

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NEMEC, J.: RANSDORF, J.

Antivibration coatings and their use. P 521

STROJIRENSTVI (Ministerstvo tezkeho strojirenstvi, Ministerstvo vscobecneco strojirenstvi) Praha, Czechoslovakia Vol. 9, no. 7 July 1959

Monthly List of East European Accessions (EEAI), LC. Vol. 9, no. 2, Feb. 1960

Uncl.

S/274/63/000/001/005/020 **D469/D308**

AUTHOR: Respect Jaros Lav

TITLE: A source of sound signals used for measurements

PERIODICAL: Referativnyy shurnal, Radiotekhnika i elektrosvyas', no. j. 1965, 8, abstract 1861 P (Csech. pat., cl. 21 e2, 10; 21 a2, 16/05, no. 100107, Jul. 15, 1961)

The patent describes a source of sound signals with a constant rate of sound flow, independent of frequency and suitable for measurements of attenuation of sound waves in accoustical absorbers and for the determination of resonant frequencies of accoustical systems. The vibrating element of the source should oscillate with speed amplitude which does not depend on frequency. The source consists of an excitation loudspeaker (EL) and a radiation loudspeaker (RL) placed in front of it in the same compartment. The membrane of the RL is excited by the accoustical field of the EL, acting on the back of the RL membrane. The back of the RL membrane. The back of the RL membrane. The back of RL is covered so that the sound produced does not affect the measurements. The space between

Card 1/2

A source of sound s	ignals	S/274/63/000, D469/D308	/001/005/020	
the front of the EL tude of voltage dev be used to measure tage may be applied tor and hence to the is maintained at a or on the associate tion of such a sour Labstracter's note	elcped across the accustical speed to an amplifier ell so that the constant level and accustical medical is described.	ne vibrating coil of sound propagate with variable amperated amplitude or and does not depend from . An example of	f the RL may ion. This vol- Lification fac- f vibrations on frequency	
Gard 2/2				

8/058/63/000/003/100/104 A066/A101 MINE. Mine, Jerelle Mifflers and their use for silenaing the noise of engines JUNEAR PERIODICAL: Referetively shurnel, Pimike, no. 3, 1963, 60, abstract 3Zh362 ("Sb. Cesimel, věd. techn. společn zdravotní techn. a vzduchotechn. CHAVE, no. 4, 1962, 43 - 65, Csech; Russian, English French and German aumaries) TEXT: Some acoustic principles proved to be highly valid in solving the noise problem of engines or compressors, especially of their exhaust. Several designs of sufflers were therefore examined both theoretically and experimentally Calculated data and results of measurements are presented. Nomograms are given for calculating the outoff frequency of an accustic filter. The methods of laboratory measurements curried out to test various versions are specified. Particular attention is devoted to a longitudinal transmitting filter and its version giving the lower outoff frequency. This type of suffler is very useful for reducing the noise of an engine exhaust. In order to give a practical example, Card 1/2

Mufflers and t	flore and ther use for		8/058 A066/	8/058/63/000/003/1 A066/A101		
ine presidentie disolot under	charteteristic	e of the miffle	r used in the 381	建设设施		
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Card 2/2						

HAUER, Josef; HAVEL, Stanislav; NENEC, Jaroslav; STEPANEK, Stanislav

Pressure vessel of the first Czechoslovak nuclear power plant.

Jaderna energie 10 no.9:322-336 S '64.

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NEMEC, Jaroslav

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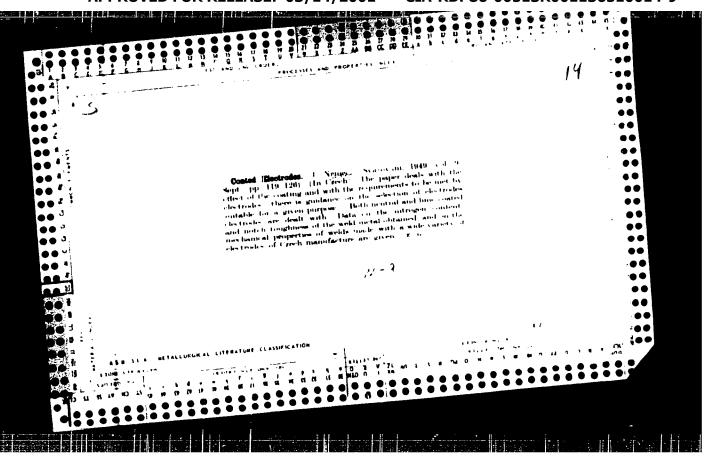
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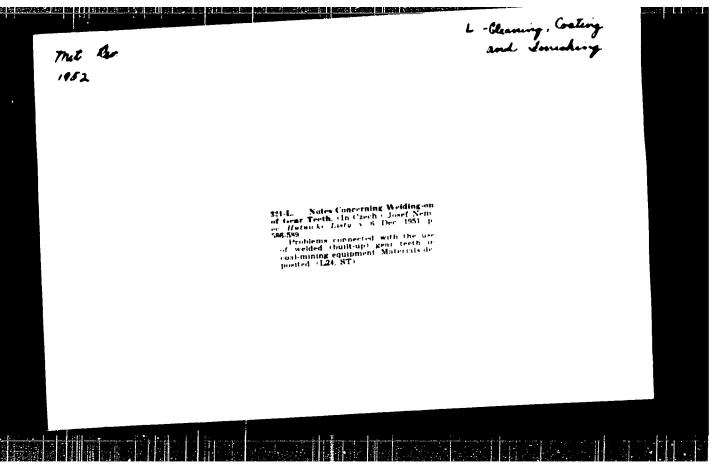
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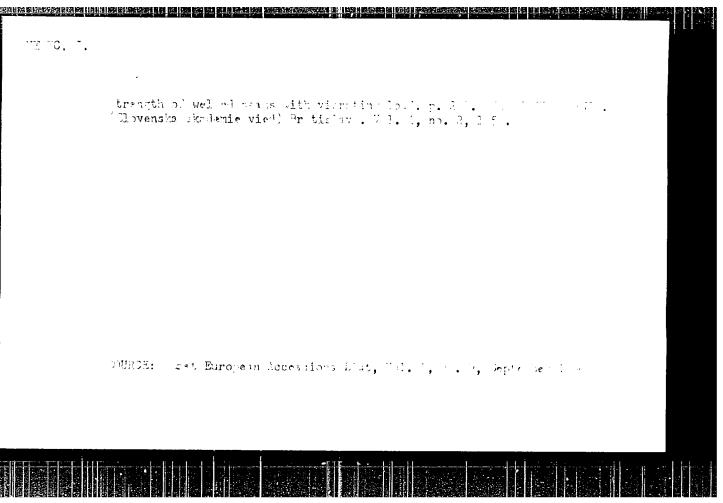
Czechoslovakia

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